Maritime Applications of Wire Arc Additive Manufacturing



ABSTRACT

Additive Manufacturing (AM) is a process where components are created by continually adding material one layer at a time. Several benefits of "additive" manufacturing versus traditional "subtractive" machining processes include a reduction of material waste, ease of producing complex parts by reducing the amount of production steps, and the reduction of manufacturing lead-time. The Wire Arc Additive Manufacturing (WAAM) process, which uses Metal Inert Gas (MIG) welding, is demonstrated to analyze its potential application for maritime utilization. This report shows how the flexural yield strength of welded plates changes with different amounts of metal additive reinforcement. A standard three-point bending test was conducted to determine the difference in flexural yield strength and to observe material behavior. Finally, it is discussed that AM processes, such as WAAM, are still being developing but their potential in the maritime industry, especially for the benefit of bringing supplies to our warfighters overseas, is clear.

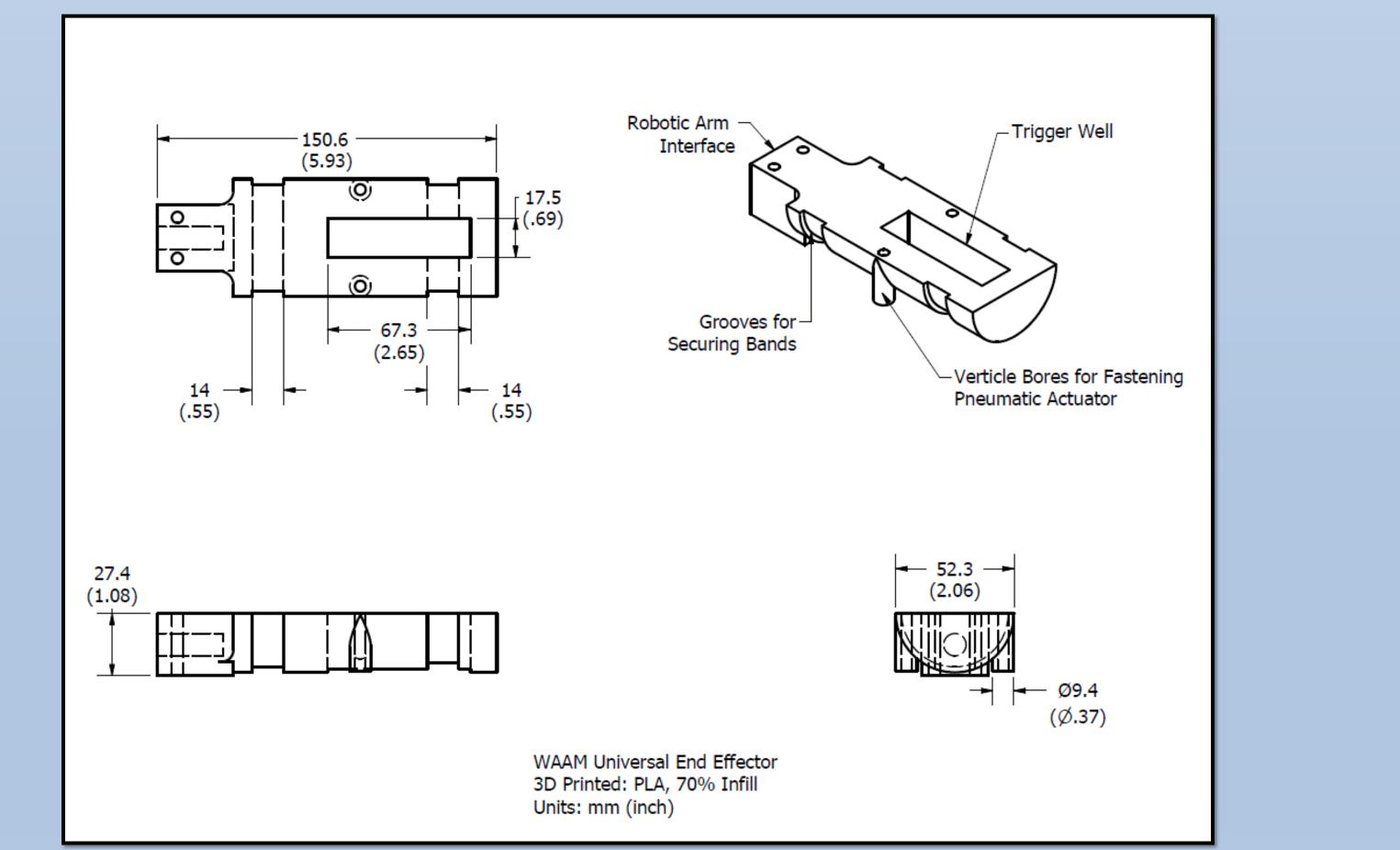
INTRODUCTION

Wire Arc Additive Manufacturing (WAAM) is a Directed Energy Deposition (DED) processed defined in ISO/ASTM52900 as the "process in which focused energy is used to fuse materials by melting as they are being deposited". WAAM is the term used for all arc welding wire-based additive manufacturing processes. WAAM and its use in the maritime industry can have practical applications onboard vessels such as printing replacement parts for mission critical engineering systems, as well as in shipyards for designing, prototyping, as well as fabricating actual end use parts such as propellers. This report analyzes the use of WAAM to reinforce metal plates using an industrial robot, MIG welder, and student-designed and 3D printed parts. A homemade robotic welding 3D printer was designed and used to place additive layers on 1018 steel plates. Six metal plates had one weld bead and another six metal plates had two weld beads placed on them (one on top of the other) by the robotic welding 3D printer. In addition, six metal plates with no weld beads were used as a control for analysis. The 3-point bending flexure test was performed with an Instron machine to analyze the flexural properties of each of the weld plates. Finally, hardness testing was conducted and stress-strain curves were created to determine the flexural yield strength of each of the metal plates.



Design of End Effector and WAAM System

A universal end effector was designed to fit most standard MIG welding guns and attach to an existing industrial robot arm. Over two design iterations, a final design was chosen that uses pipe clamps as securing bands and a pneumatic actuator which is controlled by the robot's control system to press the MIG gun trigger. Fused deposition modeling (FDM) style 3D printing was chosen as the method of manufacturing the end effector because of its ease of use and availability. A pneumatic actuator was chosen to allow the MIG gun trigger to be actuated without disassembling and re-wiring.





The WAAM system consists of an industrial robotic arm, programmable control system, 3D printed end effector, welder actuation system, and MIG welder. This system is equipped with ScoreBase operating software, a five axis robotic arm, controller unit, a teach pendent, and communication wiring. A computer and monitor connect to the PLC device via USB wiring and the PLC device connects to the robot by serial communication. The end effector connects the robotic arm to the welding gun and allows the robot to move with five degrees of freedom. The welder is a Metal Inert Gas (MIG) welder manufactured by Lincoln Electric.

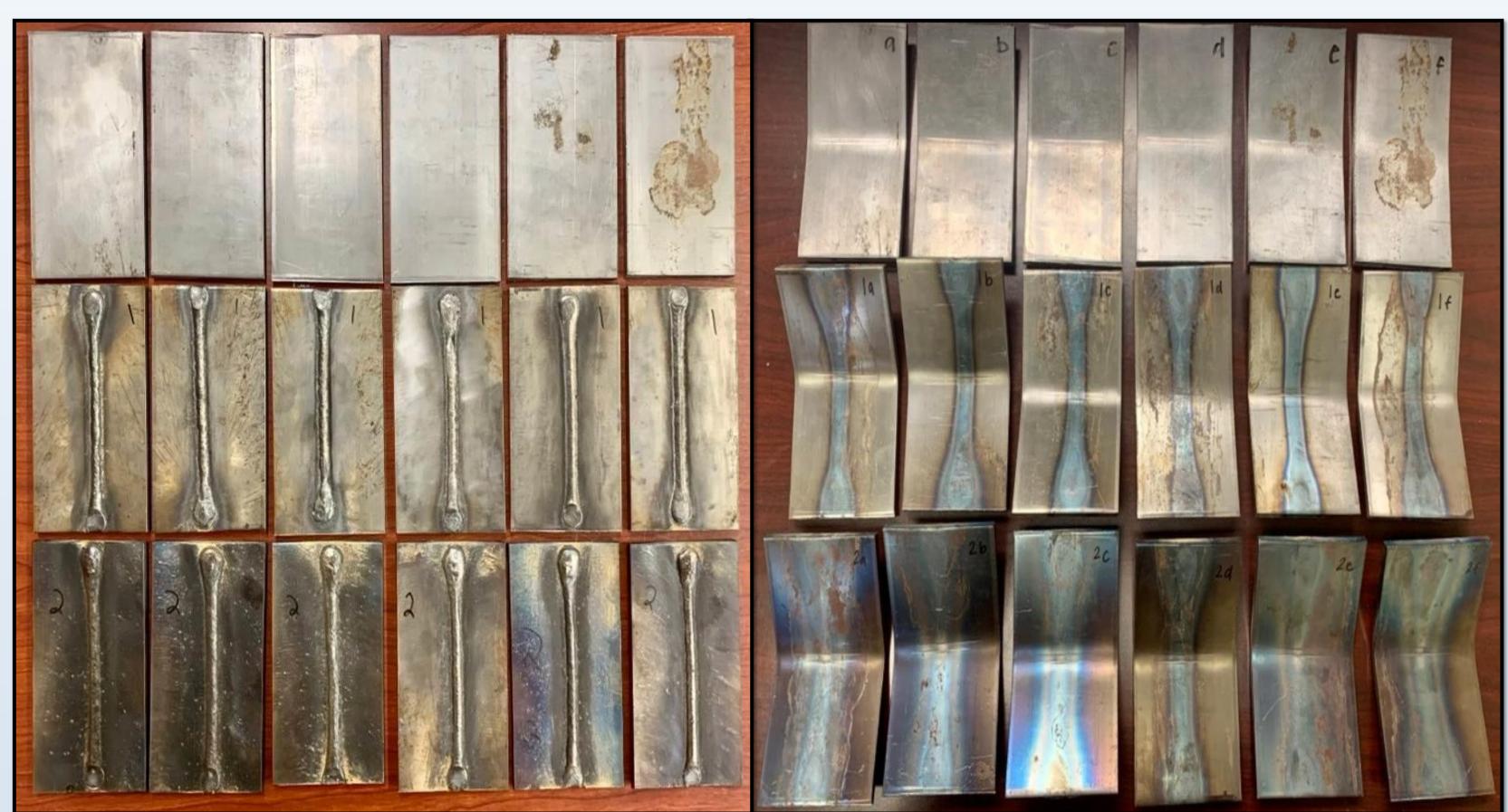
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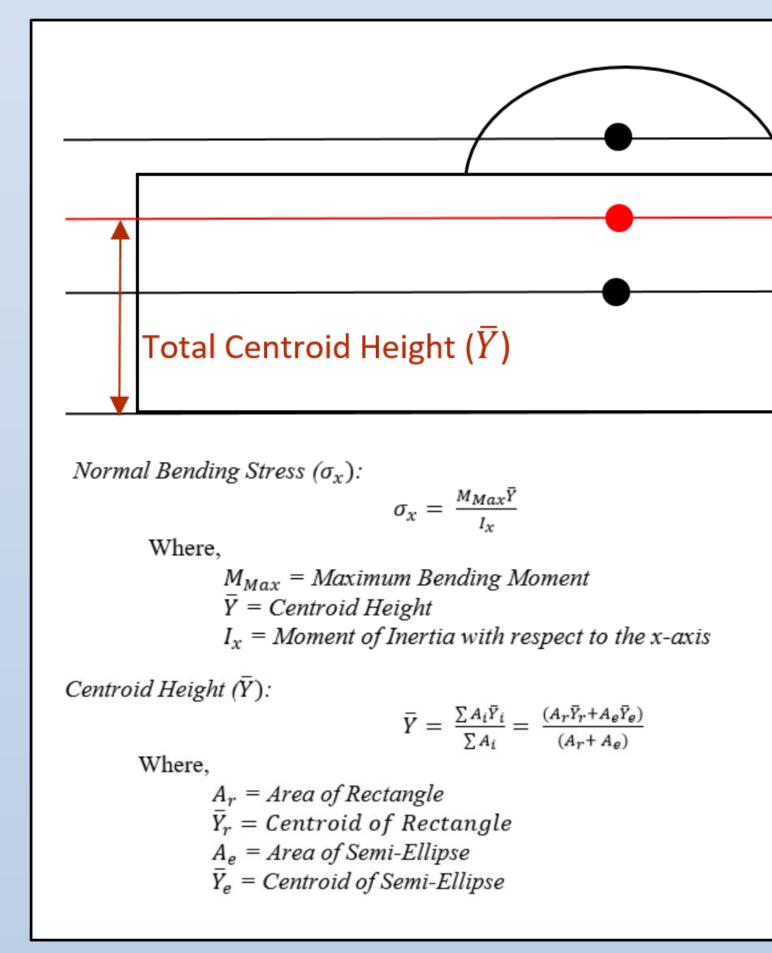
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EXPERIMENTAL DESIGN AND THEORY

In the experiment, the WAAM 3D printer was used to put additive weld beads on metal plates. The different types of metal plates are one weld bead, two weld beads (one on top of the other), and a control plate with no weld beads. There are six metal plates for each of the three types of metal plates. The flexural strength and ductile behavior of the metal plates with various weld beads can be determined from the analysis of data from a standard 3-point bending test. The procedure used for the test was followed in accordance with ASTM D790 standard for performance of flexural tests.

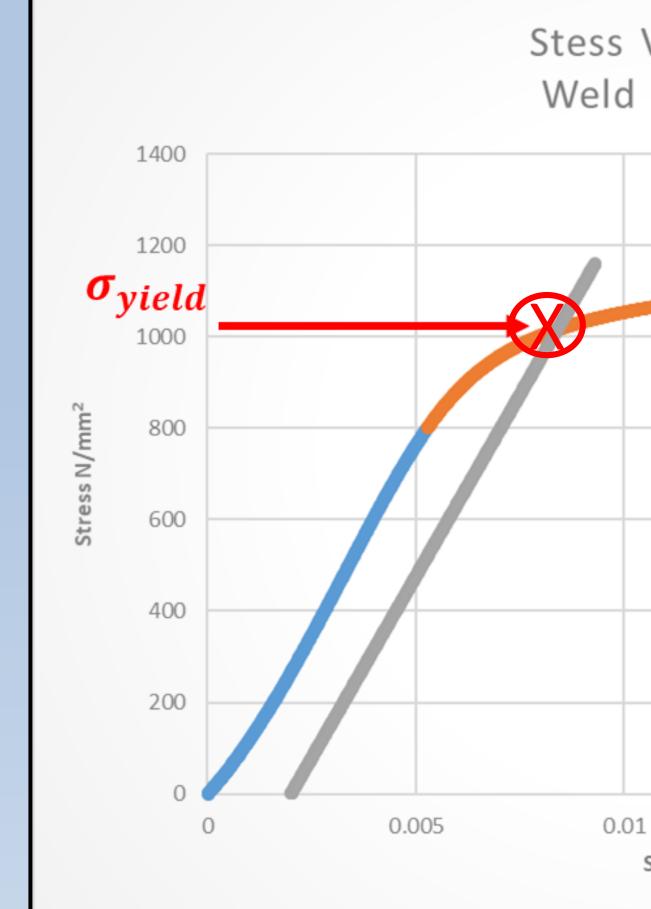


The cross section of the weld plates were modelled as rectangles with the weld beads being modelled as half-ellipses on the surface. Using the parallel axis theorem, the centroids of each shape was calculated and combined to get the total centroid height of the cross section for use in the bending stress equation for development of stress-strain curves.



EXPERIMENTAL RESULTS

After the stress and strain for each metal plate was calculated, the data was plotted to make a stress-strain curve for each of the metal plates. The figure below shows one example of the stress-strain graph for weld plate #0-f. After the stress and respective strain was calculated for each data point, the 0.2% offset method was used to help extrapolate the flexural yield strength for each of the metal plates. The blue portion of the graph is the elastic (linear) region of the deformation curve. The slope of the linear portion was determined and used to create the 0.2% offset line. The offset line is horizontally offset by 0.2% (Strain of 0.002) from the origin and parallel to the elastic region of the graph. The orange portion of the graph is the plastic deformation of the metal plate. After the linear portion of the graph was determined and the 0.2% offset line drawn, the flexural yield strength was extrapolated using the intersection of the 0.2% offset line and the stress-strain curve.



↓ d _e	Weld Bead Centroid (\overline{Y}_e)					
↓ d _r	Rectangle Centroid (\overline{Y}_r)					
Parallel Axis Theorem for Calculating I_x :						
$I_{x} = \sum (I_{n} + Ad_{n}^{2})$ = $(I_{r} + A_{r}d_{r}^{2}) + (I_{e} + A_{e}d_{e}^{2})$						
Where, $I_x = Moment of Inertia of an Area with respect to the x - axis$ $I_n = Moment of Inertia of the Area with respect to the centroidal axis parallel to the x-axis A = Area of objectd_n = distance between two axesand,I_r = Moment of Inertia, Rectangle (metal plate)A_r = Area of Rectangled_r = distance between the centroid of the metal plate with weld and the centroid of the rectangle I_e = Moment of Inertia, Semi-Ellipse (weld bead)A_e = Area of Semi-Ellipsed_e = distance between the centroid of the metal plate with weld and the centroid of the semi-ellipse$						

VS Strain Plate Of			
0.0 Strain (mm/mm)	15	0.02	0.025

The flexural yield streng for the metal plate wit respectively. The flexur The reason for this could
Weld Plat No Welds 0a 0b 0c 0d 0e 0f
Rockwell Hardness – B E18 hardness standard
Weld Plat No Welds
The temperature of the treatment can be perference material strenge weld plate can be see column shows the weld on the welds can be exactly welds.
In this experiment, the e was welded. The steel These material propert controlled cooling. No properties of the metal welder. With less volta properties of the metal reinforcement or create quality and life of the metal to note the material pro
Through extensive literal WAAM in particular, has processes that can be be done with many typ Modelers. Fabrication of the same FDM modele Finally, fabrication of ac as WAAM. As with any consumable materials to because it is a relatively part dimensions compa
 Additive manufacturing — General pri 7 Families of Additive Manufacturing. Stereolithography: The First 3D Printin https://www.asme.or ISO/ATSM 52900. International Stand Baker, Ralph. Mathod of Making Deco Strickland, J. Applications of Additive I 2016. DeVisser, K. Qualification and certifica E. Nicholls, W. Han, J. Davis. Additive Professional Project Krassenstein, B. Denmark Shipping O Damen. World's first class approved https://archive.dam A. Josten, M. Hofemann,. Arc-weldin Richard G Budynas, J. Keith Nisbett Why Post-Weld Heat Treatments Are Jonnie Liew Zhong Li, Mohd Riza All Malaysia : Center of Kirlin, Kolbe. Design and Testing of V Stress-Strain Curve: Strength of Mat diagram/. Li, Johnnieew Zhong. Review of Wire
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WARFIGHTER INNOVATION IN SCIENCE & ENGINEERING

EXPERIMENTAL RESULTS (Cont.)

VIIDAL VIELD STRENGT

igth for each of the metal plates is shown below. The average flexural yield strength th no welds, one weld, and two welds is 1000 MPa, 930 MPa, and 823 MPa, iral strength of the metal plates decreased as the welds were added to the plate. uld be the welding material and the temperature of the weld.

FLEXURAL YIELD STRENGTH				
Yield Strength (MPa)	Weld Plate 1 Weld	Yield Strength (MPa)	Weld Plate 2 Welds	Yield Strength (MPa)
1000	la	990	2a	845
1000	1b	950	2b	845
1000	1c	900	2c	820
1000	1d	910	2d	830
1000	1e	930	2e	800
1000	1f	900	2f	800
1000	Average :	930	Average :	823

tests was performed on the metal plates after welding, in accordance with ASTM procedure. This test determines the hardness of the plates, as seen below.

HARDNESS ROCKWELL B					
Plate ds	Hardness	Weld Plate 1 Weld	Hardness	Weld Plate 2 Welds	Hardness
	96	Next to Weld	95	Next to Weld	94
	97	Next to Weld	96	Next to Weld	98
	96	Next to Weld	102	Next to Weld	100
		Next to Weld	99	Next to Weld	99
		On Weld	91	On Weld	87
		On Weld	99	On Weld	80
		On Weld	92	On Weld	86
		On Weld	101	On Weld	80

e weld can affect the hardness and the flexural strength of the metal. A heat ormed after welding, called Post Weld Heat Treatment (PWHT) to maintain or gth and material properties. The drastic temperature change of the weld onto the en in the discoloration of the weld plates after welding. The figure in the center I plate discoloration on the underside of the weld plates. The decreased hardness explained by the additional temperature changes with the one weld and the two

EXPERIMENTAL CONCLUSIONS

effects of changing properties of 1018 steel were seen and analyzed after the steel changed in its material properties including hardness and flexural yield strength. ties changed because of the high temperatures of the welding process and unpost-weld heat treatments were performed in an attempt to maintain the material plates. The temperature of welding can change by changing the voltage of the ge, the temperature of welding will decrease, and this could mean the material al could be maintained. When using metal additive manufacturing to add tools/objects, the material properties need to be understood in order to predict the aterial. For practical applications of WAAM in the maritime industry, it is important operties of metal after welding additive metal layers.

MARITIME APPLICATION CONCLUSIONS

ature research and experimental work, it is shown that Additive Manufacturing, and as a clear future in the maritime industry. There are a great many types of AM used for many applications within the industry. Prototyping for design work could es of printers but are most easily and inexpensively utilized by Fused Deposition of mission critical replacement parts while on ship are also being investigated using ers but there is potential to use other newer technologies and different materials. tual end-use parts are being realized with the help of metal AM technologies such type of technology, the trick is knowing the limits of each individual machine and hat are at your disposal. WAAM has a particularly good fit in the maritime industry y inexpensive technology for printing metals (steel) and can print in relatively large red to desktop sized modelers currently on the market.

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